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TRANSPORT OF LIQUEFIED HYDROGEN: RISK ANALYSIS OF THE UNLOADING PROCESS AT THE SHIP TERMINAL *TRANSPORTE DE HIDRÓGENO LICUADO: ANÁLISIS DE RIESGOS EN EL PROCESO DE DESCARGA EN LA TERMINAL DE BUQUES*

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TRANSPORT OF LIQUEFIED HYDROGEN: RISK ANALYSIS OF THE UNLOADING PROCESS AT THE SHIP TERMINAL



WHY?

Environmental protection and the fight against climate change have driven the search for sustainable fuels, with hydrogen standing out as a promising alternative due to its high energy density and clean combustion. However, its storage and transport present significant safety challenges, especially in its liquefied form (LH2), due to its low boiling temperature and low heat of vaporization. Ensuring its safe use is key to its deployment in sectors such as energy and transport.

HOW?

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To minimize the risks associated with hydrogen storage and transport, risk analysis methodologies such as HAZOP, HAZID and FMEA are applied. These tools allow hazards to be identified, potential system failures to be assessed and preventive measures to be designed. Their implementation helps to optimize the safety and viability of hydrogen as an energy carrier, ensuring its sustainable and reliable development on a large scale.



Risk Assessment Methodologies



Risk Management is essential Advanced safety protocols are key Innovative research is crucial



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DESCRIPTION:

The vessel considered in this study is a Liquid Hydrogen Carrier (LHC) with a capacity of approximately **160,000 m³** and an overall length of approximately **300 meters**. The LHC will transport the liquid at approximately -253°C, atmospheric pressure and a ratio of liquid/gas volume of approximately 800 times.

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This vessel is based on real vessels such as the Suiso Frontier as well as others that are in the project and design phase, although the size of the vessel is larger than those currently built, and it is a theoretical model that responds to a volume comparison of current LNG carriers.





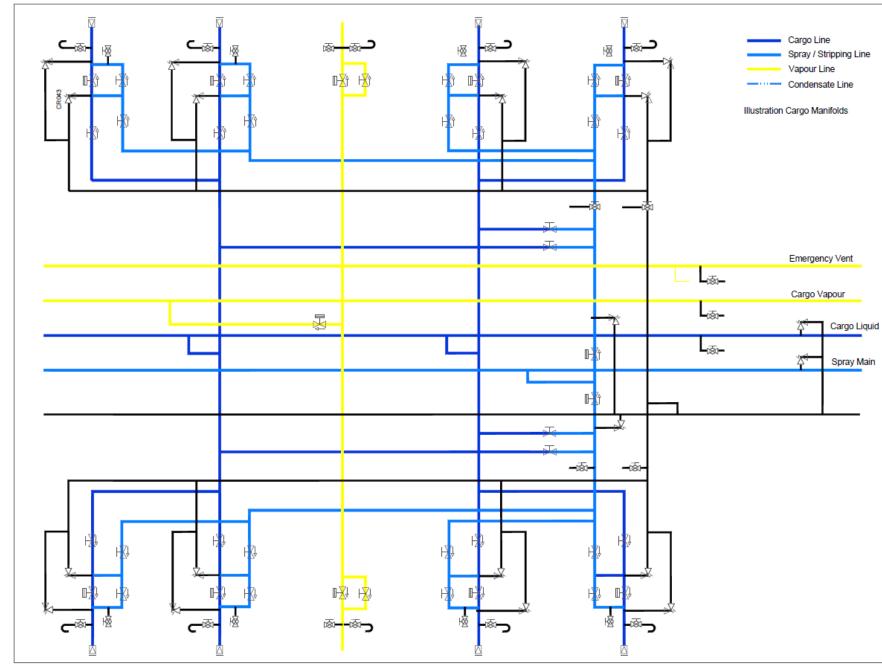
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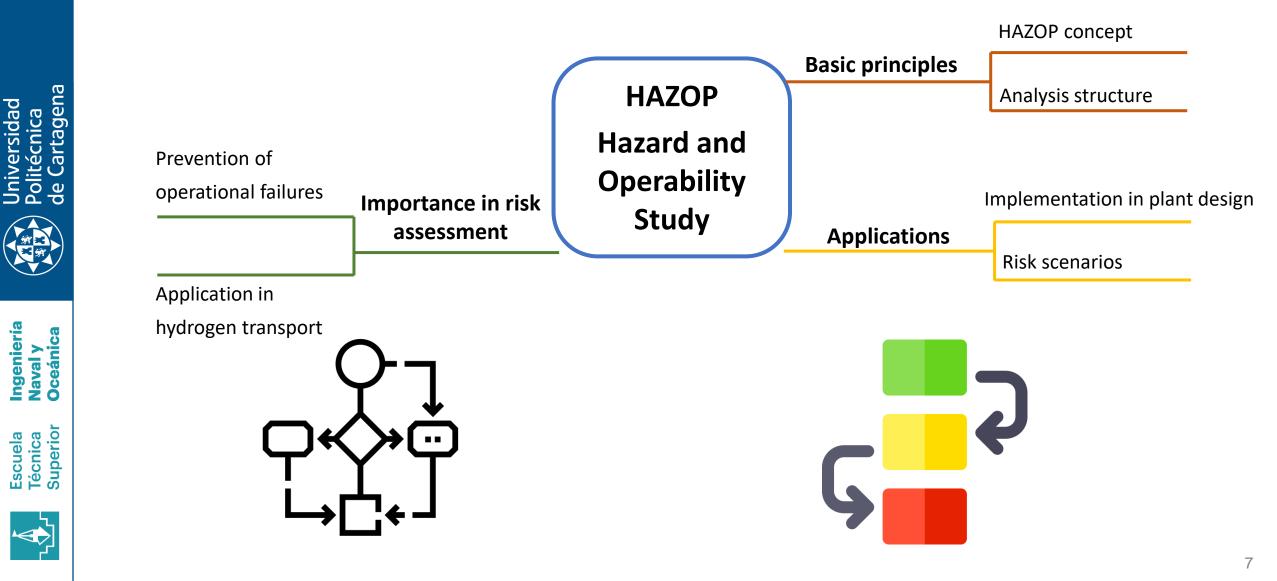




HAZOP

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HAZOP METHODOLOGY

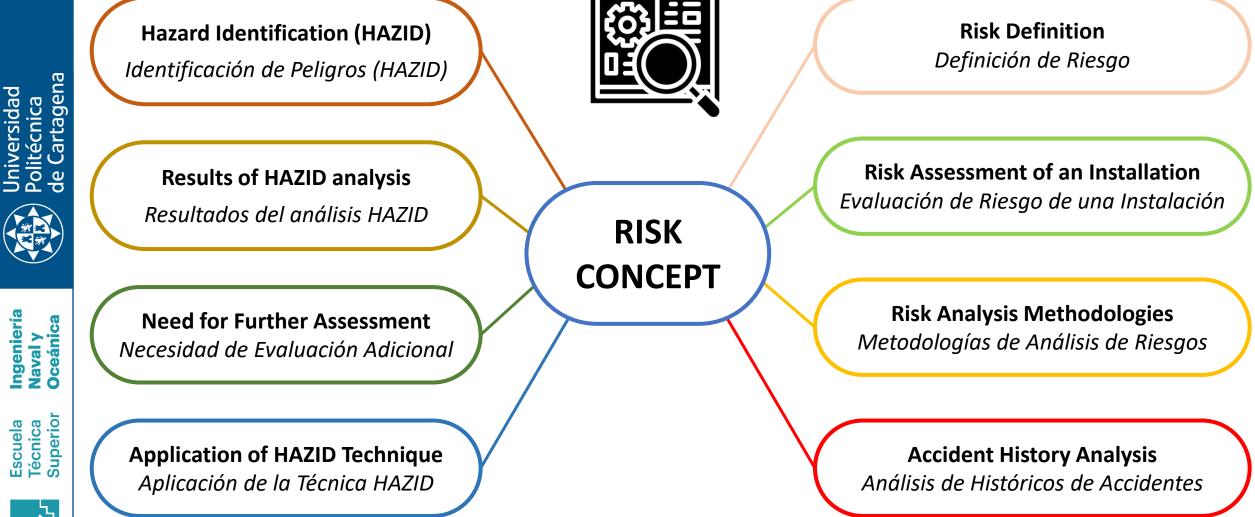






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HAZID METHODOLOGY



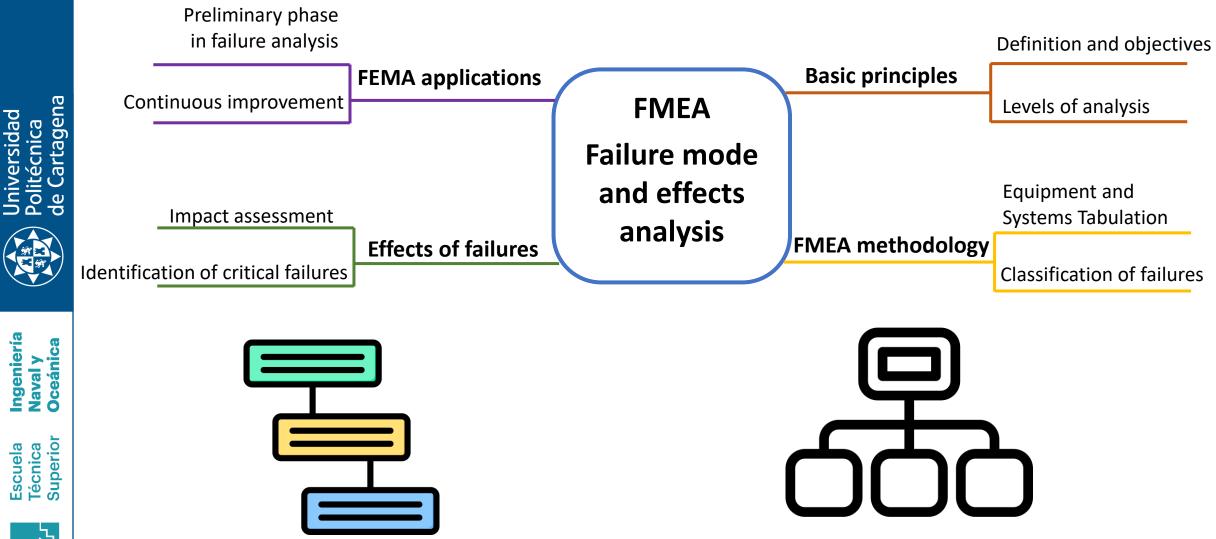






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FMEA METHODOLOGY





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HAZOP: Use Case



Case	Parameter word	Guide Word	Pos	sible cause of deviation	Consequence	CONSEQUENCE	PROBABILITY	RISK	-	
1	Flow in pipe LH2. Operat	on 1 NO LH2 Spray Pump malfunction		No fluid circulation due to pump malfunction. No cool down of required lines.	1	3	3			
2	2 Flow in pipe LH2. Operation 1 NO		Hydraulic Valves Failed to Open: Failed to open CS301		No fluid circulation due to hydraulic valves closed. No cool down of required lines.	; 1	2	2		
3 Flow in pipe LH2. Operation 1 NO		Hydraulic Valves Failed to Open: Failed to open CS303		No fluid circle to nyaratine clos of down of required lines.	1	2	2			
4	Flow in pipe LH2. Operat	ion 1 NO	Hydraulic Valves Failed to Open Failed to open CS071/072		o fluid setion in liquid crossover. No common of required lines.	1	2	2		
5	Flow in pipe LH2. Operat	ion 1 NO	Hyd	Iraulic ESD Valves leak	Possible creation of explosive atmosphere	5	3	15		
1	Operator Intervention	Independent safeguards	Prio	ity Recommended action	Comments to recommended action		Mitigation Contingency	CONSEQUEN	CE PROBABILI	п
oump runn ecirculatio	an see no fluid circulation & signal of ing. Operator should control fluid on to tank and try to restore spray pump y or start another spray from other tank.	Control system will identify sequence fi pump malfunction	ailure or Med	Check Alarms of Spray Pump Pumps and piping systems (interconected) redundancy	A se system routing the ability to pump from the other able to continue cooling the system and not ga		Contingency	0	3	
Operator ca	an see no fluid circulation & alarm no r no flow at any section line.	Control system will identify sequence f and send Trip Spray pump.	ailure Med	Check Hydraulic system Valves. Check autor sequence.	discharge p immediately to to avoid a possible lease that does not open.	e hydraulic valve at anded to emergency outic valve that does not open e flange upstream of the CS301		0	1	
	an see no fluid circulation & alarm no r no flow at any section line.	Control system will identify sequence f and first open CS300 to recirculate LH2 t if opening value CS300 failed then Trip pump. The final safeguard is to open m the CS304. Recirculation valve CL304 sho open during cooldown lines.	o tank, Spray Janually	C' fic system 8 seck automation v.ce.	S not a serious operational situation since it simply does discharge from the tank outlet line. First the recirculation th roreseen and if not a logical protection for not having circulatic valve and the pump running, the pump should be commanded and thus avoid an overpressure upstream of the hydraulic valve a possible leakage through the LH2 flange by the flange upstre not open.	rough the CS300 line should be on downstream of the hydraulic to emergency stop immediately t that does not open and avoid	Mitigation / Contingency	0	1	
Operator ca lines	an see no fluid circulation in crossovers	Automatically open CS300 to recirculate tank to avoid overpressure in cross over		ić system & Hydraulics Va ck automatic logic sequence.	This is not a serious operational situation since it simply does s that distributes the LH2 to one side of the vessel or the other in should first be made for recirculation through the line from the recirculation to the tank is not possible and the pump running, commanded to emergency shutdown immediately and thus avo crossover and prevent a possible leak through any of the LH2 fl	n the crossover. Provision CS300 to the tank and if the pump should be id overpressure in the	Mitigation / Contingency	0	1	-
close hydra	an see alarm hazardous gas detection & aulics valves CS071/CS072 to isolate te on line prior to ESD Valve	Function logic that close CS071/CS072 if hazardous gas leak is detected	gas Hij	h Isolate with manual valve this conection to shore	This is a high risk situation. To quantify the risk, it would be in amount of gas that could escape through the internal leakage us by quantifying the amount of H2 in the section considered con valve and a simulation of gasification on deck from this valve. It these risk points during operation. Provide for inspections and maintenance of critical valves.	teresting to quantify the of the valve. It could be known ning from the previous cut-off	Mitigation / Contingency	4	2	

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HAZOP: Example scenarios



Node 1 field and record selection

	CASE	POSSIBLE CAUSE OF THE DEVIATION	CONSEQUENCE	RISK
versidad itécnica Cartagena	 Flow rate in LH2 pipeline. Operation 1 - No flow 	Leakage at flange or fitting	Possible creation of an explosive atmosphere.	15
Unive Polité de Ca	2. Flow rate in LH2 pipe.Operation 1 - Excessive flowrate	LH2 pump malfunction	Excessive flow circulation. Process out of parameters	15
Escuela Ingeniería Técnica Navaly Superior Oceánica	5. H2 steam pipe flow - Excessive flow rate	Overheating	Excessive vapour in the system, action should be necessary to liquefy the vapour or burn it off.	20





RESULTS: HAZOP RISK MATRIX



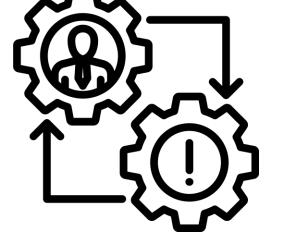
			FREQUENCIES				AFTER			FRI	EQUENC	IES			
		-	1 2 3 4 5		IMPROVEMENTS		1	2	3	4	Ī				
ad a ena		1	39	19	25	0	0			1	63	15	9	3	
/ersidad técnica Cartagena		2	12	13	15	0	0			2	20	53	13	0	
Universidad Politécnica de Cartagen	SEVERITY	3	13	36	2	0	2		SEVERITY	3	6	11	2	0	
		4	0	11	5	0	0			4	10	110	6	5	
		5	0	77	80	6	0			5	24	5	0	0	











TOTAL INITIAL							
Green	172						
Yellow	95						
Red	88						

TOTAL	AFTER
Green	227
Yellow	123
Red	5





HAZID: Example scenarios



SCENARIO 1: DEVELOPMENT	CONSEQUENCES	RISK			
D	amage to persons.				
Possibility of line breakage and supply hose D	amage to equipment or elements				
	possible cascading failures).	15			
LH2. Worst case scenario risk of fire or explosion.	amage to the environment due to				
C	ontamination.				
SCENARIO 1: CONTRO	L MEASURES				
Limit of unloading operations according to port reg	ulations. Breakaway system (ERS).	8			
Continuous monitoring by the ship. Periodic check of the mooring system (checklist).					
SCENARIO 3: DEVELOPMENT	CONSEQUENCES				
Design line pressure between ESD valve and dry	Damage to persons.				
coupling exceeded due to loss of instrumentation a	Damage to equipment or elements				
	" (possible cascading failures).	20			
in the valves. Mechanical integrity at risk with LH2	Damage to the environment due to				
leakage and possibility of fire or explosion.	contamination.				
SCENARIO 3: CONTRO	L MEASURES				
ESD warning on local panel. Operator must stop op	eration.	15			







RESULTS: HAZID RISK MATRIX

RISK = FREQUENCY x SEVERITY

	RISK MATRIX		FREQUENCIES						
			1	2	3	4	5		
INITIAL	1	1	0	0	0	0	0		
MATRIX		2	0	0	1	2	11		
	SEVERITY	3	0	1	7	4	22		
		4	0	2	4	2	3		
		5	0	11	22	3	0		

	RISK MATRIX		FREQUENCIES						
MATRIX			1	2	3	4	5		
AFTER		1	2	1	4	15	19		
IMPROVEM	SEVERITY	2	1	15	3	5	2		
		3	4	3	0	0	1		
ENTS		4	15	5	0	0	0		
		5	19	2	1	0	0		





TOTALIZERS							
RED	52						
YELLOW	41						
GREEN	2						



TOTALIZERS							
RED	2						
YELLOW	14						
GREEN	101						



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- Risk Analysis for LH2 Unloading Operations
- **Key Risks Identified**: Hydrogen leaks, ignition and explosion hazards, overpressure, cryogenic system failures, and atmospheric oxygen liquefaction.
- Mitigation Measures:
 - System segmentation with automatic valves and pressure relief systems.
 - Automation and control with interlocks and redundancy in sensors.
 - Overpressure management and evacuation circuits.
 - Continuous monitoring of the vacuum in cryogenic pipes.
- Results:
 - HAZOP: Reduced high-risk scenarios from 88 to 5.
 - HAZID: Reduced high-risk scenarios from 52 to 2.
 - FMEA: Qualitative failure identification.



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CONCLUSIONS AND FUTURE LINES



• Conclusions:

Enhanced safety through advanced leak detection, compartmentalization, and GCU redundancy.

Further quantitative risk analysis, including the application of machine learning techniques, is needed for critical scenarios.

• Future Lines:

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New tools based on Artificial Intelligence, own developments.



FIN 3

La industria naval y marítima como motor de la economía azul. Por un futuro sostenible para todos.





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Thank you very much for your attention - Muchas gracias por su atención -

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